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Naghma Hall

**APPLICATION FOR
UNITED STATES LETTERS PATENT**

FOR

**A METHOD AND APPARATUS FOR A MULTI-COMPONENT
INDUCTION INSTRUMENT MEASURING SYSTEM FOR
GEOSTEERING AND FORMATION RESISTIVITY DATA
INTERPRETATION IN HORIZONTAL, VERTICAL AND DEVIATED
WELLS**

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Background of the Invention

Cross Reference to Related Applications

5 This application is a continuation in part of U.S. Patent Application serial number 09/922,393 entitled "Multi-Component Induction Instrument" filed on August 3, 2001 by Otto N. Fanini and Stanislav W. Forgang. This application is related to and claims priority from U.S. Patent Application number 09/471,289, entitled "Apparatus Accurately Measuring Properties of a Formation" by Otto N. Fanini, Stanislav W. Forgang and Michael S. Crosskno, filed on
10 December 24, 1999. This application is related to and claims priority from U.S. Provisional Patent Application number 60/361,570, entitled "Method and Apparatus for the use of Multicomponent Induction Tool and Cross Component Measurements for Geosteering and Formation Resistivity Data Interpretation in Horizontal Wells" by Abbas Merchant, Otto Fanini, Berthold Kriegshauser and Liming Yu, filed on March 4, 2002.

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Field of the Invention

 The present invention relates to the field of induction resistivity in frequency or time domain measurements for evaluation of potential hydrocarbon bearing formations and assisting drilling and well placement decisions with geo-steering and geological information above, below
20 and ahead of the bit using downhole induction instruments having reinforced metal mandrel (monitoring while drilling-MWD) or significant amounts of electrically conductive parts in or around the sensor section. The present invention provides for compensation of eddy currents induced in the tool body, which create additive error signals that interfere with resistivity measurements for automatically estimating dip angle through joint interpretation of multi-array
25 induction and electromagnetic measurements (including high frequency "dielectric" or wave

propagation ones), multi-component induction measurements for geosteering and open hole applications involving anisotropic formations.

Summary of the Related Art

5 Electromagnetic induction resistivity well logging instruments are well known in the art. These induction resistivity well logging instruments are used to determine the electrical conductivity, or its converse, resistivity, of earth formations penetrated by a borehole. Formation conductivity has been determined based on results of measuring the magnetic field due to eddy currents that the instrument induces in the formation adjoining the borehole. The electrical
10 conductivity is used for, among other reasons, inferring the fluid content of the earth formations. Typically, lower conductivity (higher resistivity) is associated with hydrocarbon-bearing earth formations. The physical principles of electromagnetic induction well logging are well described, for example, in, J. H. Moran and K. S. Kunz, Basic Theory of Induction Logging and Application to Study of Two-Coil Sondes, Geophysics, vol. 27, No. 6, part 1, pp. 829-858,
15 Society of Exploration Geophysicists, December 1962. Many improvements and modifications to electromagnetic induction resistivity instruments described in the Moran and Kunz reference, supra, have been devised, some of which are described, for example, in U. S. patent no. 4,837,517 issued to Barber, in U. S. patent no. 5,157,605 issued to Chandler et al. and in U.S. patent no. 5,600,246 issued to Fanini et al.

20 The conventional geophysical induction resistivity well logging tool is a probe suitable for lowering into the borehole and it comprises a sensor section and other, primarily electrical, equipment for acquiring the data to determine the physical parameters that characterize the formation. The sensor section, or mandrel, comprises induction transmitters and receivers

positioned along the instrument axis and arranged in the order according to particular instrument specifications. The electrical equipment generates an electrical voltage to be further applied to a transmitter induction coil, conditions the signals coming from receiver induction coils, processes the acquired information. The acquired data then has been stored or by means of telemetry sent to the earth's surface through a wire line cable used to lower the tool into the borehole.

In general, when using a conventional induction logging tool with transmitters and receivers (induction coils) having their magnetic moments oriented only along the borehole axis, the hydrocarbon-bearing zones are difficult to detect when they occur in multi-layered or laminated reservoirs. These reservoirs usually consist of thin alternating layers of shale and sand and, oftentimes, the layers are so thin that due to the insufficient resolution of the conventional logging tool they cannot be detected individually. In this case the average conductivity of the formation is evaluated.

Thus, in a vertical borehole, a conventional induction logging tool with transmitters and receivers (induction coils) oriented only along the borehole axis responds to the average conductivity that combines the conductivity of both sand and shale. These average readings are usually dominated by the relatively higher conductivity of the shale layers. To address this problem, loggers have turned to using transverse induction logging tools where transmitters and receivers (induction coils) have their magnetic moments oriented transversely with respect to the tool longitudinal axis. The instrument for transverse induction well logging was described in U.S. patent no. 5,781,436 issued to Forgang et al.

In the transverse induction logging tools the response of transversal coil arrays or inclined coil arrays with a transverse component is also determined by an average conductivity, however, the relatively lower conductivity of hydrocarbon-bearing sand layers dominates in this

estimation. In general, the volume of shale/sand in the formation can be determined from gamma-ray or nuclear well logging measurements. Then a combination of the conventional induction logging tool with the transversal induction logging tool can be used for determining the conductivity of individual shale and sand layers.

5 One of the main difficulties in interpreting the data acquired by a transversal induction logging tool is associated with its response vulnerability to borehole conditions. Among these conditions there are a presence of a conductive well fluid as well as well bore fluid invasion effects. A known method for reducing these unwanted impacts on a transversal induction logging tool response was disclosed in L. A. Tabarovsky and M. I. Epov, Geometric and Frequency
10 Focusing in Exploration of Anisotropy Seams, Nauka, USSR Academy of Science, Siberian Division, Novosibirsk, pp. 67-129 (1972) and L. A. Tabarovsky and M. I. Epov, Radial Characteristics Of Induction Focusing Probes With Transverse Detectors In An Anisotropic Medium, Soviet Geology And Geophysics, 20 (1979), pp. 81-90.

 The known method has been used a transversal induction logging tool comprising
15 induction transmitters and receiver (induction coils). By irradiating a magnetic field the induction transmitter induces currents in the formation adjoining the borehole; in turn, the receivers measure a responding magnetic field due to these currents. To enable a wide range of vertical resolution and effective suppression of the unwanted borehole effects, measurements of magnetic from the formation can be obtained at different distances between the transmitter and
20 receiver. However, even with these modifications, the data logs obtained with a conventional transversal induction logging instruments can be inconsistent, difficult to interpret, and the problems have been exacerbated while logging through a sequence of layers.

In the induction logging instruments the acquired data quality depends primarily both on parameters of the environment the tool operates in and on its intrinsic instrument its electromagnetic response characteristics. Thus, in an ideal case, the logging tool measures signals induced only by eddy currents excited in the formation by the primary magnetic field of the induction transmitter. Variations in the magnitude and phase of the eddy currents occurring in response to variations in the formation conductivity are reflected as respective variations in the output voltage of induction receivers. In conventional induction instruments these receiver voltages (or currents floating in the receiver coils) are signal conditioned and then processed using analog or digital phase sensitive detectors, primarily - algorithmically. The processing allows for determining both receiver voltage or current amplitude and phase with respect to the induction transmitter current or its magnetic field waveforms.

As in an open hole induction logging, the induction instruments currently deployed in monitoring while drilling (MWD) operations typically utilize solenoid-type transmitter and receiver induction coils coaxial with the tool mandrel. These instruments produce a "classical" set of induction measurements in the propagation mode, measuring attenuation and phase shift in the transmitted magnetic field due to the influence of the adjacent formation. Known induction tools utilize two coaxial receiver coils positioned in the center of the mandrel and two sets of balanced transmitter coils on both sides of the receiver coils. This balanced coil configuration, when operating at two frequencies of 400kHz and 2MHz, enables the typical known induction instrument to quantitatively evaluate eight directional horizontal formation resistivities for a plurality of investigation depths.

As a general rule for induction tool design, a high degree of magnetic coupling between the tool transmitter and the formation and the tool receiver and the formation is desirable. This

high magnetic coupling between the tool transmitter/receiver and the formation facilitates increased instrument efficiency and increased overall signal to noise ratio and increases desirable sensitivity to formation parameters. However, the presence of conductive bodies typically found in the mandrel of known induction instruments becomes problematic, resulting in appearance of an additional and unavoidable magnetic coupling between these bodies and different sources of electromagnetic radiation\reception. Primarily, parasitic magnetic coupling between the transmitter, receiver and formation from one side and the conductive metal parts of the downhole tool from another side creates problems associated with parasitic eddy currents induced on the tool body surface and internal tool surfaces.

The parasitic eddy currents flowing on the surface of the downhole tool produce undesirable magnetic fields that interact with resistivity measurements as additive error components. These induced magnetic fields reduce the overall transmitter moment, couple directly into the receiver coil(s) and create undesirable offsets in measurement signals. Moreover, eddy currents on the tool body are temperature and frequency dependent that makes their adverse effects difficult, if not impossible to account and compensate for by known methods. Thus, there is a need for a method and apparatus that reduces and compensates for the adverse effects of eddy currents. Any remaining effect of the eddy currents can be calibrated out in an air calibration of a tool.

The relative formation dip angle is vital for proper and accurate interpretation of data acquired by the new multi-component array induction instrument. This newly developed induction instrument comprises three mutually orthogonal transmitter-receiver arrays. These configurations allow for determining both horizontal and vertical resistivities of an anisotropic formation in vertical, deviated, and horizontal boreholes. A description of the tool can be found

in WO 98/00733, *Electrical logging of a laminated formation*, by Beard et al (1998). The transmitters induce currents in all three spatial directions and the receivers measure the corresponding magnetic fields (H_{xx} , H_{yy} , and H_{zz}). In this nomenclature of the field responses, the first index indicates the direction of the transmitter, the second index denotes the receiver direction. As an example, H_{zz} is the magnetic field induced by a z-direction transmitter coil and measured by a z-directed receiver where the z-direction has been conventionally parallel to the borehole axis. In addition, the instrument measures all cross-components of the magnetic fields, i.e., H_{xy} , H_{xz} , H_{yx} , H_{yz} , H_{zx} , and H_{zy} . In general inductive measurements can also be made in any non-orthogonal directions, for example, 20 and 40 degrees off or an orthogonal direction.

The signals acquired by the main receiver coils (H_{xx} , H_{yy} , and H_{zz}) are used to determine both the horizontal and vertical resistivity of the formation. This is done by inverse processing techniques of the data. These inverse processing techniques automatically adjust formation parameters in order to optimize in a cost-function for example a least-square sense measuring the data mismatch of the synthetic tool responses with measured data. Required inputs in this process are accurate information of the relative formation dip and relative formation azimuth. This information can be derived using in addition to the main signals (H_{xx} , H_{yy} , and H_{zz}) from the cross-components.

Conventional induction tools comprising only coaxial transmitter-receiver coil configurations do not have azimuthal sensitivity. Therefore, in a horizontal wellbore, the data does not contain information about directionality of the formation. It is not possible to distinguish whether a layer is above or below the borehole from these data alone. There is a need to be able to determine directionality of the formation. This knowledge can be obtained

using a subset or all of the cross-components of the new multi-component induction tool that allows for determination of directionality of the formation.

Summary of the Invention

5 The present invention provides improved measurement capabilities for induction tools for formation resistivity evaluations and geo-steering applications. The present invention provides electromagnetic transmitters and sensors suitable for transmitting and receiving magnetic fields in radial directions that are orthogonal to the tool's longitudinal axis with minimal susceptibility to errors associated with parasitic eddy currents induced in the metal components surrounding
10 the transmitter and receiver coils. The present invention provides increased effective tool surface impedance by increasing self-inductance of the paths in which induced eddy currents flow on the surface of the multi-component induction instruments.

 The present invention enables downhole tool designers to build more effective and better-protected radial induction arrays for existing and future downhole instruments operating in the
15 frequency and/or time domains. In this case the array measurement results contain information primarily about the formation's vertical resistivity. Moreover, the present invention also makes it possible to combine transverse arrays with longitudinal arrays which conventionally measure horizontal formation resistivity or other directionality arrays. This combination enables obtaining a full resistivity tensor to evaluate formation resistivity anisotropy.

20 In one aspect, the present invention provides a composite non-conductive housing to reduce or even avoid the effects of parasitic eddy currents flowing on the tool surface. In another aspect, the present invention provides a conductive non-magnetic housing with reduced effects of conductive materials near coils and, primarily, the receiver. In another aspect of the

invention, a non-conductive coating is placed over the housing to prevent high frequency eddy currents from leaking from the housing in the conductive mud of the adjacent wellbore and returning back to the housing.

In one aspect of the present invention inserts with certain material properties (conductivity, permeability and dielectric) and outer shell openings with special shapes and magnetic lenses combined with a transverse magnetic path are provided. In another aspect of the present invention an azimuthally symmetric measuring system combining an outer shell opening, shield, and coil placed on surface of the tool comprising a magnetic material or wound around magnetic material, transverse magnetic path, mud column are provided.

In another aspect of the present invention an azimuthally asymmetric measuring system combining outer shell opening, shield, coil placed on surface of magnetic material or wound around magnetic material, transverse magnetic path, mud column is provided. In yet another aspect of the present invention system configurations utilizing discontinuous parts of an equivalent cylindrical magnetic path, magnetic fields measured at high and low frequency and electric field sensors combined with outer shell opening with special shapes. In yet another aspect of the present invention, transmitter and receiver arrays with openings implemented with measuring system including features listed above. The present invention also provides a method for application to geo-steering operations.

The present invention provides a method that uses measurements for geo-steering applications. Measurements could be performed either in a time domain being then optionally converted into frequency domain with selecting a spectrum of interest, or performed in the frequency domain itself. The tool provides a tuned, broadband or re-tunable coil(s) and a tuned, broadband or re-tunable source. The present invention provides opening sizes and geometry of

the tool. The tool openings can be varied dynamically to change the direction of sensitivity and frequency response of a transmitter or coil adjacent the above mentioned opening. The tool also provides a multi-layer flexible circuit board containing at least one of a coil, a selectable shield, a magnetic layer and tunable components. The tool also enables dual compensated measurement of
5 array to improve signal to noise ratio and measurement stability and to improve signal content with reservoir, geological and geophysical information. The tool utilizes methods for application for geo-steering, drilling assistance and decisions. The tool provides a transverse magnetic path and in general any magnetic path combination which occurs in whole or in part in a transverse plane perpendicular to the tool longitudinal axis. The tool method utilizes multiple frequency
10 sequential or simultaneous measurements and time domain measurements. The tool method utilizes measurements of an array combined with gyro, accelerometer, magnetometer and inclinometer data at same time.

Various transmitter-receiver combinations distributed azimuthally around the tool or longitudinally are provided to select sensitivity to a desired reservoir formation properties, for
15 example, different orientations xy , xz , yz , 20° - 40° , 40° - 90° , and combinations, such as, Symmetric – symmetric; Asymmetric – symmetric; and Asymmetric – asymmetric to help direct the sensitivity of the tool to a desired direction.

The present invention also provides a method of using a multi-component resistivity logging tool in a deviated, highly deviated or substantially horizontal borehole. Using at least
20 data recorded in a single receiver with two different transmitter orientations and vice versa due to a reciprocity, it is possible to determine the direction of resistive beds relative to the borehole. When multi-frequency measurements are used, the present invention also makes it possible to

determine a distance and direction to the resistive bed and formation anomalies such as a fracture or discontinuity in the bed.

Brief Description of the Drawings

5 **Figure 1** illustrates circumferential direction of eddy currents that will flow on the surface of the conventional induction MWD instrument with a longitudinally-oriented transmitter magnetic field propagating along the longitudinal axis of the tool body;

Figure 2 illustrates a preferred embodiment with a coil that is wound around a tool body inside of collar and has a magnetic moment directed along the tool longitudinal axis body;

10 **Figure 3** and **Figure 4** are side views of a preferred embodiment illustrating radial and longitudinal ferrite inserts to minimize eddy currents on the tool surface flowing due to a radial transmitter field;

Figure 5 is an illustration of a conductive housing interfering with a transmitted magnetic field in the case when tool housing also contains ferro-magnetic inclusions;

15 **Figure 6** is an illustration of a ferrite insert inside of a coil shaping the magnetic flux outside the instrument and in close proximity to a tool surface;

Figure 7 is an illustration of a preferred collar surrounding a coil;

Figure 8 is an illustration of a preferred collar surrounding a coil;

Figure 9 is an illustration of a preferred collar surrounding a coil;

20 **Figure 10** is a cross sectional area of the coil and collar of **Figure 9**;

Figure 11 illustrates a preferred tool external side view along longitudinal axis showing longitudinal apertures traditionally used in previous resistivity propagation tools;

Figure 11A illustrates a cross-section of a preferred tool showing outer shell, shields, transverse magnetic path and internal mud flow section;

Figure 12 illustrates external tool's side view along tool longitudinal axis showing transverse apertures aligned with transverse plane perpendicular tool longitudinal axis.

5 **Figure 13** illustrates external tool's side view along tool longitudinal axis showing apertures in a transverse plane varying its orientation from a direction perpendicular to the tool axis towards a direction aligned with the tool's longitudinal axis;

Figure 14 illustrates external tool's side view along tool longitudinal axis showing apertures with a circular shape including aperture gaps in the circular direction;

10 **Figure 15** illustrates Cross-section of tool illustrating geometry and dimensions of a insert to the tool's external surface;

Figure 16 illustrates External tool's side view along tool longitudinal axis showing annular apertures. One annular aperture (left) is placed in transverse plane perpendicular to tool's longitudinal axis. The other annular aperture (right) is placed in transverse plane whose direction
15 is inclined (between 0 and 90 degrees) with respect to the tool's longitudinal axis;

Figure 17 illustrates Description of aperture shape with the form of a "time capsule" profile. One particular shape has both extremities with a conical cut and the center has a restriction with a parallel cut. An alternate shape has cuts at both the extremities which are parallel to each other. Lateral cuts are curved and could have a circular, elliptic or parabolic
20 shapes, for example with center outside cut;

Figure 17A illustrates Description of key dimensions in one of the "time capsule" shapes;

Figure 18 illustrates Aperture with an elliptic shape;

Figure 19 illustrates Aperture shape has the form of a parallelogram(left) and alternatively one parallelogram in each extremity of the aperture united by a restriction of parallel cuts;

Figure 20 illustrates Aperture shape like a “bone”. Extremities have a shape resembling a circular shape united by a “neck” restriction;

Figure 20A illustrates Aperture shape like a “bone”. Extremities have a shape resembling an elliptic shape united by a neck restriction;

Figure 21 illustrates Aperture shape like a cross shape combining cuts in a longitudinal and transverse direction with respect to the tool’s longitudinal axis;

Figure 22 illustrates Tool’s side view along the tool longitudinal axis showing description of a sequence of apertures (each represented by a line) which are varying their direction and are organized longitudinally (left side example) and another case where the aperture’s directions are varying and are organized azimuthally(right side example); Apertures could alternatively be organized within a plane with direction inclined to the tool longitudinal axis;

Figure 23 illustrates switches that are connected within the aperture and can change dynamically the geometry and dimensions of the aperture. An example of a cross-cut is shown but this can be extended to other shapes;

Figure 24 illustrates an example showing an aperture whose effective dimensions and shape have been reconfigured with switches that can be extended to other shapes;

Figure 25 illustrates standard apertures. Aperture can be inclined by an angle θ with respect to the tool longitudinal direction;

Figure 26 illustrates an aperture with time capsules shapes. The aperture can be inclined be an angle θ with respect to tool longitudinal direction;

Figure 27 illustrates comparative relative attenuations through the aperture with “time capsule” shape and standard aperture opening versus angle between direction of aperture and direction incident magnetic field projected on tool external surface where aperture is cut. Each relative attenuation has been normalized to 1 at θ equal to 0 for comparison of spatial direction selectivity between the two aperture geometries;

Figures 28-72 illustrate preferred coil, apertures, inserts and shield configurations;

Figure 73 depicts a sketch of the new 3DEX multi-component induction tool developed by Baker Hughes;

Figure 74 shows an example of two simulated cases of horizontal formations;

Figure 75 shows a graph of a typical six-level anisotropic turbidite sequence along with responses of the five components to the applied RF magnetic field at 20 kHz;

Figure 76 shows a graph of a six-level isotropic sequence along with responses of the five components to the applied RF magnetic field at 20 kHz;

Figure 77 shows a graph of the sequence of **Figure 76** with altered resistivities at the first bed layer along with responses of the five components to the applied RF magnetic field at 20 kHz;

Figure 78 shows a graph of the sequence of **Figure 76** with altered resistivities at the sixth bed layer along with responses of the five components to the applied RF magnetic field at 20 kHz;

Figure 79 shows a graph of a three-level linearly graded transition sequence along with responses of the five components to the applied RF magnetic field at 20 kHz;

Figure 80 shows a graph of a thick resistive bed sandwiched between two conductive beds along with responses of the five components of the applied RF magnetic field at 20 kHz;

Figure 81 shows a graph of a thick conductive bed sandwich between two resistive beds with responses of the five components of the applied RF magnetic field at 20 kHz;

5 **Figure 82** shows the five component responses to the applied 200-kHz RF magnetic field as the invention is rotated through 180 degrees inside a horizontal borehole within the second bed of **Figure 76**;

10 **Figure 83** shows the five component responses to the applied 20-kHz RF magnetic field as the invention is rotated through 180 degrees inside a horizontal borehole within the second bed of **Figure 76**;

Figure 84 shows a multi-component 3DEX induction configuration of the invention for vertical wells.

Figure 85a shows a plot of a model of formation resistivity against logging depth, with three anisotropic resistivity intervals;

15 **Figure 85b** shows a model of the responses of H_{xx} and H_{zz} in both isotropic and anisotropic materials of **Figure 85a**;

Figure 86 shows a multi-component induction configuration of the invention for horizontal wells;

20 **Figure 87** shows a configuration for a horizontal well application used to obtain results shown in **Figure 74**; and

Figure 88 shows a configuration for a horizontal well application used to obtain results displayed in **Figures 75-83**;

Figures 89-92 illustrate binning of formation data;

Figure 93 illustrates a preferred time averaging equation; and

Figure 94, the raw data assigned to a depth interval and azimuth sector can fall in different points of the repeat cycle.

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Detailed Description of a Preferred Embodiment

The transmitter and receiver coil geometric areas together with the transmitter current define a total magnetic moment of an induction tool. By design, these coils are built preferably with an effective geometrical area sufficiently large to achieve the maximum possible random noise-free measurements while using conventional amounts of electrical power available to MWD equipment. A coil effective geometric area would be sufficiently large when non-productive losses that may occur while generating the primary magnetic field or detecting the secondary magnetic field flux induced from the formation are either adequately compensated for or properly accounted for. In many circumstances these limitations can be evaluated from the basic physics principles, i.e., from boundary conditions for the magnetic field being in a close proximity to a conductive and/or ferromagnetic materials or propagating along these parts.

It is known from the electromagnetic field science that if an externally generated alternating magnetic field has been radiated normally to the surface of a conductive body, it will induce eddy currents on this surface. These currents, in turn, produce their own magnetic fields that, in vector sense, oppose to the external field. Generally, the opposing field magnitude increases with increasing material electrical conductivity and decreases with increasing distance to the source. These result in the fact that an integral magnetic flux in a close proximity to a highly conductive metallic surface becomes negligible. For those who are skilled in the art it

should be understood that similar effects are present in induction MWD instruments having transmitter and receiver coils wound in a close proximity to the metal tool body.

Hence, when a transmitter induction coil is positioned right above a conductive tool surface, the magnetic field of eddy currents induced on the surface opposes the primary source and thus decreases the integral flux radiated into the formation. Conversely, if a receiver induction coil is positioned above a conductive surface, the magnetic field of eddy currents induced on this surface due to formation response will decrease an effective flux crossing the coil. Both processes substantially distort receiver output voltage and, consequentially, lower the tool signal-to-noise ratio.

In the most practical tool designs, the wavelength of the transmitter field is significantly longer than the electromagnetic skin depth of the tool body material or the coil linear dimensions. This fact allows for neglecting active electromagnetic losses in the tool body materials, disregarding phase shifts between surface eddy currents and the driving magnetic field, etc. Surface eddy currents decrease effective coil geometrical areas, however, when operating frequencies are too high to ignore coil dimensions and/or the tool body material losses, the eddy currents effect becomes more complex and should be analyzed separately for every logging case.

Turning now to **Figure 1**, **Figure 1** illustrates the direction of the eddy currents flowing on a tool surface with transmitter magnetic fields are oriented and propagating along the longitudinal axis of the tool body. As shown in **Figure 1**, a longitudinal magnetic field **110** is generated by transmitter and longitudinal magnetic field **120** is received by the receiver oriented along the longitudinal axis of the tool **100**. Surface parasitic eddy currents are generated in the mandrel **105** and preferably circulate on in a circumferential path along the direction **130**, as

shown in **Figure 1**. Non-conductive or highly resistive ferrite inserts **107** in the transmitter collar **109** and receiver collar **111** are utilized for two purposes. The inserts under the transmitter coil **107** increase electrical impedance of the tool surface to allow for a larger flux leak from the coil to be radiated in the formation. Inserts under the receiver coil **107** effectively increase the external field penetration through coil cross-section allowing for larger signal to be measured. Both effects occur due to known behavior of the induction coil wound fully or partially around a ferromagnetic solid. The inserts **107** reduce the effect of circumferential eddy currents on magnetic fields in collars **109** and **111**.

Preferably, the tool body is made of non-magnetic but conductive material to reduce often non-linear magnetization effects of this material on the flux transmitted and received by the tool. The tool body can alternatively be made of non-conductive composite material to completely eliminate eddy currents flowing on the tool surface. In this design case, having ferrite inserts **107** under the transmitter coil in transmitter collar **109** becomes unnecessary. Having the inserts **107** under receiver collar **111** would still be desirable for attracting more external flux lines to penetrate through its cross-section.

Turning now to **Figure 2**, coil **202** is shown wound around a tool body **100** inside of collar **109** (or collar **111**). Ferrite inserts **107** are shown embedded in the tool surface **105** and within coil winding **202**. The tool transmitter radiates in a direction along the tool longitudinal axis and, therefore, induced eddy currents **206** travel circumferentially around ferrite inserts **107** as shown in **Figure 2**. The ferrite inserts effectively increase the eddy current travel path and forces this path to exhibit a substantial inductance. The increased effective impedance encountered by the eddy currents flowing through this travel path, around the ferrite inserts, will

reduce magnitude of these currents and, respectively, downscale their parasitic effects on effective transmitted and received magnetic fluxes.

Turning now to **Figure 3** and **Figure 4**, a preferred embodiment of the present invention is illustrated which provides for placement of induction coils **310** for radiating a transmitter magnetic field in the formation or receiving respective signal from the formation. The magnetic moment of each of these coils has been perpendicular to the longitudinal axis of the tool **340** to support induction measurements from the radial direction. While operating, both primary, i.e., transmitter and secondary, i.e., formation fields mainly induce longitudinal eddy currents **330** on the surface of the tool **340**. The present invention increases the tool surface impedance not only within transmitter and receiver coil projections on the tool surface, but outside of these projections on the tool body, as well. As shown in **Figure 3**, high magnetic permeability inserts **320** are provided within the coil and outside of the coil **310** along the mandrel to reduce the effect of eddy currents **330** having different travel directions.

Thus, referring to **Figure 3**, two major currents are induced by the magnetic field of the radial coil and flowing in opposite directions. A first current is contained within the projection of the coil winding on the tool metal surface and the second current flows outside of this projection. The present invention reduces the influence of longitudinal current streams on the measurement results by providing segment type ferrite inserts **320** arranged transverse with the tool's longitudinal axis and located primarily within the coil projection on the mandrel surface as shown in **Figure 3**. Longitudinal ferrite inserts **360** are similarly placed along the mandrel primarily outside the coil projection area on the mandrel surface, as shown in **Figure 4**. These longitudinal inserts extend the path and also increase the effective impedance for circumferential streams of eddy currents traveling outside of the coil projection on the tool surface. That is,

Figure 4 demonstrates the principle of the surface eddy current suppression by means of increasing the tool surface inductive impedance. The ferrite inserts being embedded in the surface forced currents to flow in multiple loops, simultaneously increasing inductance of these loops and their impedance to the current circulation. Preferably, a plurality of longitudinal inserts
5 are provided instead of a single insert on each side of the coil. By applying similar consideration, those who are skilled in the art would find that in the case of the receiver coil used per the present invention ferrite inserts within the coil projection on the tool surface effectively increase the coil area.

In a preferred embodiment, a non-conductive coating **370** is placed over tool **340** to
10 restrict eddy currents **330** from leaking into conductive fluid filling the well bore surrounding the tool **340**. Effectiveness of the non-conductive coating depends on coating thickness and the coating complex electric permittivity. The coating effectiveness will also operate in converse with the tool operation frequency and, therefore, the coating material thickness and frequency should be selected properly. A good engineering practice would require a capacitive impedance
15 introduced by this coating between the tool surface and borehole fluid to be at least an order of magnitude higher than the integral inductive impedance the surface eddy currents experience. For those who are skilled in the art would see that these two reactive impedances may present a series resonance circuit that could destroy measurement phase stability and quality, primarily in boreholes filled with high conductivity fluids.

20 It is known that a ferromagnetic body placed in a less magnetic volume "filled" with magnetic flux lines acts as a flux concentrator, i.e., the flux lines are distorted in a way that a majority of the lines pass through the ferromagnetic body. The analogue to this effect can be found in an electrical current (flux) flowing through the circuit and selecting the minimal

electrical (magnetic) impedance to flow. In accordance with this analogue, volumes containing ferromagnetic inclusions are known as having smaller "magnetic" impedance to the flux lines spatial routing. For downhole MWD applications this means that improper coil position within close proximity to the ferromagnetic tool parts and components (such as a tool body) might significantly change MWD transmitted and received magnetic fluxes. Moreover, for some embodiments this can create an effect completely compromising the above mentioned advantages. Thus, it may result in suppression of magnetic field transmitted to and received from the formation as shown in **Figure 5**.

Figure 5 illustrates a negative effect of a tool pressure housing **402** built from magnetic material. As shown in **Figure 5**, a transmitter coil **410** has been wound on the transverse ferrite core **412** that has been positioned inside the tool metal housing and connects both external MWD surfaces **400**. Depending on the ratio of magnetic permeability of the ferrite **412** to the housing **402** one, the magnetic flux **420** can be partially or fully trapped inside the body and never leave the tool to survey the formation and vice-versa.

As shown in **Figure 6**, applications of ferrite inserts **510** in the transmitter or receiver coils **500** would have different meanings. Thus, in case of receiver coil it results in the increased magnetic flux density **520** inside the coil's core compared to the external field to be measured. If the transmitter coil current is set (as with supplying it with a "current" source), however, the presence or absence of the ferromagnetic core does not practically affect the radiated field except for some increased flux line concentration per unit of cross sectional area in close proximity to the coil. Thus, the ferrite inside of the transmitter coil serves primarily as a "container" that does not allow transmitter field flux lines to leak inside the instrument and route the flux lines in a

transverse path across the tool. In the case where ferromagnetic inserts are used for the receiver coil, they work as both a "container" and magnetic flux density magnifier.

Turning now to **Figure 7**, a preferable solution is shown which provides a non-conductive collar **600**, which, in the case of induction measurement instruments is preferably not a load-bearing collar **610**. A preferred embodiment as shown in **Figure 8** comprises a simple hollow composite cylinder **650** mounted coaxial with the instrument on the tool external surface with the coil **640** buried inside the composite collar. In this case the thickness of the collar introduces a gap between the collar **650** surface and external surface of the central pipe **620**. This arrangement enables the magnetic flux **630** to penetrate in coil leaking through the gap, i.e., between coil wires and external surface of the metal pipe.

Moreover, the composite filling the gap further comprises embedded ferromagnetic fibers **635** oriented normally to the collar surface, as shown in **Figure 10**, thereby increasing the coil effectiveness (primarily for the receiver). An inner cylindrical composite **652** is added with ferromagnetic fibers oriented along a circle in a plane perpendicular to tool axis. These fibers in this inner cylindrical composite part guide magnetic flux lines around a central structural metallic MWD component **620**. To facilitate this aspect of the tool implementation, the central structural metallic MWD component **620** is made of a non-ferromagnetic metallic material or alternatively covered with a cylindrical layer of a non-ferromagnetic metallic material. Alternatively the central structural metallic MWD component **620** could be covered with a cylindrical layer of ferromagnetic metal material providing a transverse magnetic path.

In a preferred embodiment, all radial the coil windings are preferably symmetrical with respect to the external tool surface. Also in a preferred embodiment, longitudinal coil windings and split coils have the same axis of symmetry as the tool itself by design. The overall benefits of

symmetrical windings in induction tool are known in the art and have been supported by numerical modeling results and experimental field data. In case of MWD instruments, in particular, the asymmetrical windings cause non-symmetric eddy currents traveling in different locations in the instrument. Being parasitic, the magnetic fields due to these currents are almost impossible to cancel, that is, using asymmetrical windings would result in unwanted signal pick-up and cross-talk between coils, distortion of the tool's calibration and introduce the data interpretation difficulties.

In a preferred embodiment, the radial transmitter and receiver coil are each wound around the tool surface, having an even number of turns and symmetrically wound, that is, half of the coil windings going on one side of the tool and the other half - on the opposite side. In this case the radial coils provided inside of the collar, are symmetrically wound so that their total magnetic moment in the axial direction is substantially equal to "zero".

Figures 11 through 27 describe the inserts and openings provided by the present invention. The inserts and openings' function would be primarily to allow electromagnetic energy to leak through the tool metallic outer shell in both directions for either a transmitter or a receiver. There are three groups of characteristics for the inserts and openings comprising a combination with a parallel grid shield and a transverse magnetic path across the tool body, material properties, and shape.

The present invention provides a novel combination of a parallel grid shield and a transverse magnetic path across the tool body. The present invention provides an insert specification which includes the joint implementation of an insert, shield and magnetic path. This is a hardware solution which contains the basic functions for a measuring system: means to leak electromagnetic energy through the metallic outer shell (openings/insert); parallel grid shields to

improve sensor's directional selectivity to the field orientation of interest; transverse magnetic path. This is shown to the right of **Figure 11**. Various inserts shapes including longitudinal, transverse, deviated, curvilinear, and annular shapes which are shown in **Figures 11, 12, 13, 14,** and **16**. If this is not sufficient to obtain a claim allowance then it is necessary to resort to the shape of the opening and material properties of what is placed within the opening/insert what is discussed next. An example for an aperture with dynamically adjustable shape and dimension is also illustrated herein.

Figure 15 illustrates characteristics of inserts, which have contrasting characteristics (i.e. conductivity, permeability, dielectric) with respect to the surrounding outer shell material.

In a one embodiment of the present invention the material characteristics of the insert are magnetic and/or non-lossy (ferrite). The depth of the insert can also vary from a thin sheet to the whole outer-shell thickness.

Figure 16 illustrates an external tool's side view along tool longitudinal axis showing annular apertures. One annular aperture (left) is placed in transverse plane perpendicular to tool's longitudinal axis. The other annular aperture (right) is placed in transverse plane whose direction is inclined (between 0 and 90 degrees) with respect to the tool's longitudinal axis.

The present invention also provides a variety of opening shapes to be considered as shown in **Figure 17** (conical and time capsule), **Figure 17a** (conical), **Figure 18** (elliptical), **Figure 19** (diamond and double-diamond), **Figure 20** (bone), **Figure 20a** (bone), **Figure 21** (cross-cut), **Figure 22** (longitudinal and transverse opening arrays) **Figure 23** (adjustable cross-cut ratio), **Figure 24** (cross-cut ratio example), **Figure 25** (standard longitudinal example), **Figure 26** (time capsule example), and **Figure 27** (directional sensitivity improvement). **Figure 27** illustrates how the transmission directional selectivity of magnetic field through the opening

is altered by the different aperture shapes. This selectivity is more effective for fields near the outer shell surfaces and it would be less pronounced for field far from this surface. Directionality for the receiver and transmitter's spatial electromagnetic field sensitivities is obtained by combining opening/insert arrays organized longitudinally and azimuthally in the outer shell as shown in **Figure 59** and **Figure 22**.

The present invention also provides for magnetic lens effects. Magnetic materials are shaped like optical components such as lenses and placed in the measuring system to increase sensitivity. A magnetic lens with a concave face is placed at the external edge plane of the cylindrical outer shell as shown in **Figure 28**. These magnetic lens are coupled to a transverse magnetic path such as the case of cylindrical geometry shown in **Figure 28**. Both types of coil options are utilized, that is, a coil wound on magnetic material and a coil placed on magnetic surface).

The present invention also provides a structure for a symmetric measuring system. **Figure 29** illustrates transverse inserts combined with shields including directional focusing conductive strips on a parallel grid placed under the outer shell openings with the functionality to control the magnetic field's directions which will go through. **Figure 29** also shows the MWD outer shell, openings, cylindrical magnetic part, and a coil. **Figure 30** shows a cross-section of a symmetric arrangement using the option 2 type coil as shown in **Figure 28**. This arrangement also appears in **Figure 10**. **Figure 30** illustrates openings and inserts, combined with shields, that is, directional focus strips on both sides of the coil, a split flat and a surface coil, (option 2 type coil shown in **Figure 28**), a cylindrical magnetic portion, an outer shell, a mud flow pipe, and an inner electromagnetic shield placed around the mud pipe. **Figure 31** shows how parallel grid shields with conductive strips placed over the transverse coils can have different orientation

to effectively filter electric fields in a desired direction. **Figure 31** provides a split coil arrangement with coordinated polarities. **Figure 32** utilizes option 1 as shown in **Figure 28** (coil wound around a magnetic material). The coil shown in **Figure 28** and **Figure 32** utilizes a symmetrical split coil arrangement with coordinated polarity. Each coil in **Figure 32** is surrounded by an electromagnetic shield. The coils are wound longitudinally around the cylindrical magnetic part providing a transverse magnetic path as shown in **Figure 6**. The inserts and openings in the outer shell are also indicated. The mud flow pipe is indicated in the center. The continuous cylindrical path is suitable for a receiver but for additional functionality as required for a transmitter functionality, a pair of gaps is provided to interrupt the flux flowing through the magnetic path in order to be pushed into the formation efficiently. The pair of gaps is added to the structure of **Figure 32** to form **Figure 33** where they are marked in the drawing. **Figure 34** illustrates the extent of this gap indicating there needs to be a sufficiently high permeability contrast between the gap's material and the magnetically permeable material forming the magnetic path continuation next to it. There are one or more gaps placed along the magnetic path. **Figure 35** combines key elements of the present invention. **Figure 35** illustrates coils wound with option 1 as shown in **Figure 28**, that is, a coil wound around a magnetic material. The magnetic cylinder part is also shown in **Figure 10**. A coil wound placed on the surface of a transverse magnetic path is shown in **Figure 6** (option 1, **Figure 28**) and a coil wound on a magnetic cylinder is shown in **Figure 10** (option 2, **Figure 28**). The magnetic cylinder shown in **Figure 10** and other figures is one special case of a transverse magnetic path.

The present invention also provides an asymmetric measuring system. **Figures 36, 37 and 38** illustrate a special case of a half transverse coils. **Figure 36** illustrates a coil wound with option 2 (a coil placed along the surface of a magnetic material, that is, a surface coil). The

measuring system now uses a magnetic cylindrical shell, which provides a magnetic return path for the magnetic flux generated by the coil placed at the magnetic material's surface. In an alternative embodiment, the less active or non-active parts of the magnetic cylinder can be removed with only a magnetic cylindrical shell left. **Figure 36** illustrates inserts and openings, which enable electromagnetic energy to pass through the outer shell. The position for directional focus strips (parallel conductive grid shown in **Figure 31**) is illustrated in **Figure 36**. An axis of symmetry is also shown in this drawing. Flux density flow outside the tool is indicated. **Figure 37** shows two coils wound with option 1 (coil wound longitudinally around magnetic material) and placed symmetrically in the cylindrical shell generating flux density in opposite directions. In all other features **Figure 37** is similar to **Figure 36**. Flux density flow outside the tool is indicated. Axis of symmetry is shown in **Figure 37**. **Figure 38** is a special case of **Figure 37** where only one coil is wound around cylindrical magnetic shell. The present invention also provides for reduced transverse magnetic paths as compared to complete magnetic cylindrical shell.

As shown in **Figure 39**, a cross-section A-A of the magnetic frame illustrated in **Figure 40** and its longitudinal position also indicated in **Figure 40**. The magnetic frame provides a magnetic path found also included within in cylinder made of magnetic material as shown in previous figures. The magnetic frame as shown in the figure has two circles at each end united by two bars mounted longitudinally across from each other in opposite sides. There are two symmetric coils provided with coordinated polarities mounted on each side (I top side and II low side) of the magnetic frame. Flow of flux density is also indicated. **Figure 41a** (longitudinal opposing magnetic bars), **Figure 41 b** (coaxial rings) and **Figure 41c** (cylindrical shells) illustrate options with reduced transverse magnetic paths.

Another alternative for the setup shown in **Figures 39** and **40** is illustrated in **Figures 42** and **44**. The two symmetric coils (coil type 2, **Figure 28**) are placed in the external surface of each one of the opposing bars in the magnetic frame shown in **Figure 44** (similar to **Figure 40**) with coordinated polarities.

5 **Figures 43** and **45** illustrate a simple sketch suggesting how one, two or more coils could be mounted in the external surface of corresponding magnetic bars where they would be mounted. Figure 45 shows how three systems shown in **Figure 36** could be combined (coil type 2, **Figure 28**). **Figure 46** illustrates how three pair of coils (coil type 1, **Figure 28**) could be mounted in three cylindrical sections of a magnetic cylindrical shell separated by gaps
10 combining three coil systems shown in **Figure 37**. Similarly **Figure 47** illustrates how to combine the three coil systems shown in **Figure 38** (coil type 1, **Figure 28**). **Figures 48** and **49** show a range of relative radial positions for the split coil pair. **Figure 48** coil pairs (option 2 wound type **Figure 28**) vary their relative radial angular positions from 180 degrees (symmetric around tool longitudinal axis **Figure 30**) to 0 degree (coils coincide to form **Figure 36**).
15 Similarly **Figure 49** coil pairs (options 1 wound type – **Figure 28**) vary their relative radial angular positions from 180 degrees (symmetric around tool longitudinal axis **Figure 32**) to 0 degree (coils coincide to form **Figure 38**).

The present invention provides for electromagnetic fields measurement at high and low frequencies. **Figure 50** and **51** illustrate the fields, which typically are measurements of interest
20 at high and low frequency respectively. **Figure 50** illustrates field measurements at high frequency. In **Figure 50** for the longitudinal opening/insert the azimuthally oriented electrical field and longitudinal magnetic field are indicated. In **Figure 50** for the transverse opening/insert the longitudinal electrical field and azimuthally magnetic field are indicated. **Figure 51**

illustrates field measurements at low frequency. The main difference is the fields are of deeper penetration into the formation and are normal to the tool's opening/surface as the figure illustrates.

The present invention enables an electric field sensor to be combined with the openings
5 and inserts of the present invention. **Figure 52** illustrates longitudinal electrical field measured through a transverse opening electromagnetic window. **Figure 53** illustrates an electric field measured through a sloped opening. Similarly it has been shown how conventional longitudinal openings allow measurement of electrical field parallel to the opening (electromagnetic window). **Figure 54** illustrates a tool longitudinal cross-section with a T-shaped electric field antenna
10 under an electromagnetic window aperture placed in the outer shell. The signal detected by the antenna is brought to pre-amplifier by coaxial wire referenced to a ground producing amplified signal V_E . Mud column is also indicated. Similarly **Figure 55** utilizes a L-shape electrical field antenna instead. Similarly **Figure 56** utilizes a toroid-shaped sensor (Discussed in the open literature by Karinski at the SPWLA 2001 conference) shown aligned with a longitudinal
15 opening/insert. The tool's longitudinal cross-section A-A, shown in **Figure 57**, illustrates the toroid-shaped sensor utilizing a core with a profile having a ribbon-like, circle or oval cross-sections. **Figure 58** illustrates cross-section B-B in plane perpendicular to tool axis. Mud column pipe and outer shell are shown in **Figure 58**.

The present invention also provides measuring system with transmitter and receiver
20 arrays. **Figure 59** suggests a measurement system with a group of transmitter and receiver opening arrays. **Figure 59** illustrates one transmitter opening and two receiver openings (1 & 2). The following measurement combinations are enabled and utilized by the method and apparatus of the present invention: (i) Measure amplitude ratio of any received signal pair; (ii) Measure

phase difference of any received signal pair; (iii) any combination of receiver array aperture or openings; (iv) measurement with any order of transmitter-receiver (one or more) openings; (v) Cover any array of transmitter-receiver openings order and orientation; (vii) i through v arranged longitudinally; (vi) i through v arranged azimuthally; (viii) cross-components – different receiver orientations; and (ix) cross-components – different receiver azimuthally positions.

Turning now to **Figures 11, 12 and 13**, **Figure 11** illustrates a cylindrical tool housing **1001** having longitudinal apertures **1000**, which can either be empty or filled with an insert material. **Figure 12** illustrates transverse apertures **1002**, which can either be empty or filled with an insert material. **Figure 13** illustrates deviated apertures **1006**, which deviates more from a straight path as the aperture progresses along the longitudinal axis of the aperture, which can either be empty or filled with an insert material. **Figure 14** illustrates curvilinear apertures **1009** and **1008**, which can either be empty or filled with an insert material. As shown in **Figure 15**, a variable depth insert **1003** is shown, wherein the thickness **1005** of the insert is less than or equal to the thickness **1007** of the wall. **Figure 16** illustrates an annular aperture **1010** and an inclined annular aperture **1011**.

Turning now to **Figure 17**, the shape of the apertures affects the selectivity and attenuation of the transmitted or received fields associated with shaped apertures. For example, the attenuation pattern **1017** shown the rectangular opening **1000** of **Figure 11** has less selectivity than the attenuation pattern **1018** for the time capsule shaped aperture **1012** of **Figure 17**. Each aperture shape of the present invention provides a different and unique attenuation pattern through the outer shell for the antenna transmitter and receiver inside of the tool body. **Figures 17 and 17A** illustrates “time capsule” aperture shapes **1012, 1013 and 1014**. **Figure 18** illustrates an elliptical aperture shape **1015**. **Figure 19** illustrates a diamond **1021** and double

diamond 1022 aperture shape. **Figures 20 and 20A** illustrates additional variations 1023 and 1024 on the apertures of the present invention.

Turning now to **Figure 21**, a cross-cut aperture is illustrated, having a horizontal dimension 1025 and a vertical dimension 1026. The relation of the horizontal dimension to the vertical dimension determines the effective angle of orientation for the measured or transmitted electric and magnetic fields projection with respect to the longitudinal axis of the tool. The angle theta for the vector E_T of the electric field is given by \tan^{-1} (vertical dimension / horizontal dimension), that is $E_T = E_V + E_H$. The present invention enables high frequency, low frequency, time domain transients and frequency domain induction and propagation. Frequency domain enables measurements of fields tangential to the surface of the tool. The cross-cut enables the equivalent of a deviated aperture due to the superposition of the vertical and horizontal components.

Figure 22 illustrates a series of apertures that vary longitudinally 1032 and a series of apertures that vary azimuthally 1034, which enables aligning the axis of the measurement with the axis of a layer in the formation. In a preferred embodiment, multiple patterns are provided and one or all are utilized separately or together during transmission and or reception. **Figure 23** illustrates a cross-cut aperture that is switched to change the vertical and horizontal dimensions of the cross-cut aperture and vary the relative attenuation. The switches 1036 adjust the length of the apertures 1037 and 1038. The switch electrically shorts out the aperture and effectively changes the length of the aperture. As shown in **Figure 24**, switches 1040 are shown in the closed position and switches 1041 are shown in the open position. All switches behind a closed switch 1040 are also closed so that the effective area of the aperture is only that area occupied by the open switches 1041, up to and including the first closed switch 1040.

Figure 28 illustrates magnetic lens **1042** and two coil configuration options. Option 1 (magnetic core) is to wound a coil **1046** around a magnetic lens **1042** and Option 2 (surface coil) is to place a magnetic coil on the surface. Surface coils **1044** (type 2) are placed on surface of magnetic body **1045** and mounted with magnetic lens **1042**. **Figure 28** illustrate a mud column **1048**, and magnetic material **1045**, which continues a magnetic path from the lens **1042**. **Figure 29** illustrates a surface coil **1056** with transverse apertures and inserts **1050** and directional focus strips or shield **1051**. The field is directed according to the angular position of the directional focus strips **1051**. Outer shell is shown in **1054** and **1000** with aperture **1050**. A cross section of the configuration of **Figure 29** is illustrated in **Figure 30**. A directional focus strip or shield is placed one each side or either side of the coils **1059**. The coils are preferably split symmetrically and parallel to the cylinder **1045**.

Turning now to **Figure 32**, a coil configuration wherein coils **1060** (option 1 **Figure 28**) and shields **1080** are wrapped around a magnetic material **1062** is illustrated. Turning now to **Figure 31**, a transverse coil **1062** having a longitudinal axis parallel to the tool body is shown along with a focus strip or shield **1064**. The shield is oriented at an angle θ **1065** with respect to the longitudinal tool axis, which directs the directional field sensitivity of the coil with an angle at a preferred direction. Preferably a pattern apertures and a series of shields are coupled together to achieve a preferred field directions. The shields enhance the selectivity of the field direction associated with the apertures shapes and relational arrangements as shown above. The multiple apertures and shields can be switched to be used simultaneously or individually to obtain a directional signal. This is especially helpful in geo-steering applications. Turning now to **Figure 32**, a receiver configuration is illustrated wherein a coil **1060** is wrapped around a magnetic path. **1062**. Directional focus strips **1064** or shields are shown wherein coil **1060** is

shielded by the shields **1080** from undesirable fields. Turning now to **Figure 33**, a transmitter configuration is illustrated having a gap **1065** to enable transmission of flux into the formation. **Figure 34** illustrates gap **1065** wherein the magnetic permeability, μ_1 of the gap is much less than the magnetic permeability, μ_2 of the magnetic material **1062**.

5 Turning now to **Figure 35**, **Figure 35** illustrates a symmetrical split coil transmitter for the diminution of eddy currents, wound on a transverse magnetic path as shown in **Figure 6** and a magnetic cylinder as shown in **Figure 10**. As shown in **Figure 35**, directional focus strip **1064** and gap **1065** is provided. Turning now to **Figure 36**, an asymmetrical arrangement is shown in which only a portion of the magnetic cylinder **1045** which is most active is present and curved
10 outward to shape the magnetic field by reducing the magnetic impedance. The coil **1060** is wound outside of the existing portion of the magnetic cylinder **1045**. A directional focus strip **1045** serves as a selective shield to focus the magnetic field. **Figure 37** illustrates a dual coil **1060** arrangement wound onto the partial cylinder **1045**. **Figure 38** illustrates a single coil **1060** arrangement wound onto the partial cylinder **1045**. Note that at high frequencies, the tangential
15 field M is picked up by the structure of **Figure 38**.

 Turning now to **Figure 39**, **Figure 39** illustrates the ends **1075** of a ferrite magnetic path are illustrated. A magnetic cradle or substructure of the magnetic cylinder is illustrated in **Figure 40**. The magnetic cradle contains the coil and the magnetic flux associated with the coil. The cradle keeps the coil from touching the tool body and a transverse magnetic path contour
20 just inside the coil winding. **Figures 41A, 41B** and **41C** illustrate additional transverse magnetic path substructures of the magnetic cylinder provided by the present invention. **Figure 42** illustrates a combination of a symmetrical coil pair **1060** and magnetic frame **1075**. **Figures 43** and **44** illustrate a pair of symmetric surface coils **1060** on top of a magnetic cradle **1075**.

Figure 43 illustrates a set of three surface coils arranged on a magnetic cylinder. Thus, one, two, three or more surface coils or coils wound on magnetic centers can be used coupled together or independent of one another. **Figure 45** illustrates three surface coils **1060** with gaps **1065** separating sections of magnetic cylinder **1075**. **Figure 46** illustrates three symmetrical pairs wound on magnetic centers on sections of a cylinder sub section. **Figure 47** illustrates the single coils wound on magnetic centers on sections of a cylinder sub section. **Figure 48** illustrates three arrangements for surface coils (type 2, **Figure 28**) wherein the separation between coils is 180 degrees, $(180 - \theta)$ degrees and zero degrees. **Figure 49** illustrates three arrangements for coils wound on magnetic centers (type 1, **Figure 28**) wherein the angular separation θ **1090** between coils varies from 180 degrees to zero degrees. Thus, the present invention provides a combination of shield and a cylinder, a shield and an insert/aperture, or a shield, an insert/aperture and a cylinder. In a preferred embodiment the shield is active and switched so that the shield is selectively engaged. The switched shield enables rotation of a magnetic dipole direction for reception and transmission of magnetic flux in the tool. Aperture geometries and dimensions can be dynamically changed by switches.

Turning now to **Figure 50**, at high frequency induction shallower fields, for propagation and time domain high frequency spectra, are measured as shown in **Figure 50**, the longitudinal magnetic field, H_z **1093** is measured by the longitudinal aperture **1091**, which is parallel to the longitudinal axis of the tool **1095**, and the transverse magnetic field, H_ϕ **1094** is measured by the transverse aperture **1092**. Note that H_z has a perpendicular electric field component E_ϕ **1096** and H_ϕ has a perpendicular electric field component E_z **1097**. Turning now to **Figure 51**, at lower frequencies the deeper fields H_r are measured from the formation by a transverse magnetic path, that is H_r is measured by the longitudinal **1091** and the transverse **1092** apertures. **Figures 52**

and 53 illustrate a transverse time capsule shaped aperture 2000 and a sloped “time capsule” shaped aperture 2001 respectively.

Figure 54 illustrates a “T-shaped” antenna 2002 beneath a transverse aperture 2003 (Figure 52) utilized to measure E_z . Figure 55 illustrates a “L-shaped” antenna 2005 beneath a transverse aperture 2004 utilized to capture E_z . Figures 56, 57 and 58 illustrate a longitudinal time capsule shaped aperture 2010 for capturing electrical field E_ϕ 2013 in electric field sensor 2011. Note that the shield 2014 is formed by parallel conductors connected at one end and oriented perpendicular to the electric field being measured. Apertures 2002, 2003 and 2010 can be oriented in longitudinal, transverse or inclined directions (see Figures 52 and 53). With these aperture orientations E_ϕ , E_z and combinations of E_ϕ with E_z will be measured respectively.

Figure 59 is discussed above. Figure 59 illustrates a plurality of transmitters and receivers. The transmitters and receivers shown in Figure 59 are utilized to achieve a dual compensated measurement array. As shown in Figure 59, an array configuration comprises a plurality of transmitters, T1, T2, T3, etc. and a plurality of receivers, R1, R2, R3, etc. For example, assuming the following configuration of transmitter and receiver coils along the longitudinal axis of the tool: T1, T3, R1, R2, T4 and T2. Dual compensated measurement is accomplished by firing from T1 and making paired measurements from the remaining coils. Then firing from T2 at the other end and making a symmetric measurement from the other side. For example, when firing from T1, reception occurs at T3, R1, R2, and T4. Note that the same coil can be used as a receiver and as a transmitter, thus reception at T3 and T4 is possible. Dual compensated measurements are accomplished by measuring the ratio of the amplitudes and phase differences of the signal received at R1 and R2; R2 and T4; T3 and R1; R1 and T4; T3 and R2. Then similarly the primary signal should be fired from T2 with and receiving at T4, R2, R1

and T3. Dual compensated measurements are accomplished by comparing the ratio of the amplitudes and phase differences of the signal received at R2 and R1; T4 and R2; R1 and T3; T4 and R1; R2 and T3. Generally, firing T1 into any antenna pair combination located between T1 and T2 and firing T2 into the corresponding symmetric pair combination located between T1 and T2 could do this. Such corresponding symmetric measurements obtained from both T1 and T2 are used to compensate pressure and temperature effects on the measurements. For example, T1 is fired and the signal is measured at R1 and R2. Then T2 is fired and the response is measured at R2 and R1. A plurality of receivers and transmitters and dual compensated measurements is discussed in U.S. Patent No. 5,892,361 and U.S. Patent No. 5,574,374. In a preferred embodiment the ratio of the amplitudes measured at R1 and R2 at a given frequency is measured. In the time domain a time difference between two receivers R1 and R2 is measured and then the ratio metric time domain difference between R1 and R2 or the phase difference between the signals received at R1 and R2 has been determined. The amplitude difference in the frequency domain is measured while a single frequency is used. This method can include a plurality of frequencies. The compensated measurement improves quality of raw data and sensitivity to formation parameters enhancing data interpretation performance and results.

Turning now to **Figure 60**, illustrates an apparatus for measurement of a magnetic field in a preferred direction. As shown in **Figure 60**, a plurality of measurement coil assemblies is provided for measurement of H_0 , H_{30} , H_{60} , and H_{90} . Each coil assembly comprises a coil **2104**, an opening **2102**, and a shield **2100**. Each coil assembly is positioned to align with a particular magnetic field direction or angle. In **Figure 60**, for example, the coil assemblies are positioned to, but not limited to, align with magnetic fields at 0, 30, 60 and 90 degrees from the longitudinal axis of the tool. The directional measurements are to resolve formation geological and

reservation characteristics. A set of coil assemblies can be distributed longitudinally as shown in **Figure 60**, or distributed azimuthally.

Turning now to **Figure 61**, a coil can be implemented by multiple turns built with a multiple layer flexible circuit board. Turning now to **Figure 62**, a one piece multiple layer circuit board comprises a cross section of the flexible circuit board comprising coil turns **2108** separated by isolation/protection layers **2106**. Thus there are four isolation protection layers with a single coil turn between each pair of isolation layers. Turning now to **Figure 63**, **Figure 63** illustrates an isometric view of the flexible circuit board comprising N isolation layers and M coil turns. Turning now to **Figure 64**, a flexible circuit board further comprising a magnetic layer to serve as a magnetic cylinder and a surface coil (type 2, **Figure 28**) on top of the magnetic layer. Turning now to **Figure 65**, a flexible circuit board is shown comprising tunable and switchable components **2112** and/or magnetic lenses focusing or magnetic path **2114** mounted on the flexible circuit board. Turning now to **Figure 66**, a flexible circuit board is shown comprising a coil and a switch **2116** to make or break the coil **2108**. Thus, in the structure shown in **Figure 66**, there can be multiple coils in multiple layers and by switching one can select the direction desired for orientation of the magnetic field sensitivity. Thus, one can make or break coil turns in a single layer or in multiple layers. Turning now to **Figure 67** and **68**, a flexible circuit board housing a coil is shown having a shield **2118** layer with coil and isolation layers which can be switchable. Turning now to **Figure 69**, a coil having a coil return **2119** in a separate layer, thus the area of the coil is perpendicular to the flexible circuit board, thus, multiple turns can be contained in the plane perpendicular to the flexible circuit board. As shown **Figure 70**, the coil turns are shown with a magnetic layer between them so that the flexible circuit board now comprises a coil wound on magnetic material (type 1, **Figure 28**).

Turning now to **Figure 71** and **72**, a multiple layer flexible circuit board is illustrated having a coil return in a separate layer to form multiple coil turns. Turning now to **Figure 73**, **Figure 73** shows the configuration of transmitter and receiver coils in a preferred embodiment of the 3DEXplorer™ (3DEX) induction logging instrument of Baker Hughes. Three orthogonal transmitters **1101**, **1103**, and **1105** that are referred to as the T_x , T_z , and T_y transmitters are placed in the order shown. The three transmitters induce magnetic fields in three spatial directions. The subscripts (x, y, z) indicate an orthogonal system substantially defined by the directions of the normals to the transmitters. The z-axis is chosen to be along the longitudinal axis of the tool, while the x-axis and y-axis are mutually perpendicular directions lying in the plane transverse to the axis. Corresponding to each transmitter **1101**, **1103**, and **1105** are associated receivers **1111**, **1113**, and **1115**, referred to as the R_x , R_z , and R_y receivers, aligned along the orthogonal system defined by the transmitter normals, placed in the order shown in **Figure 73**. R_x , R_z , and R_y are responsible for measuring the corresponding magnetic fields H_{xx} , H_{zz} , and H_{yy} . Within this system for naming the magnetic fields, the first index indicates the direction of the transmitter and the second index indicates the direction of the receiver. In addition, the receivers R_y and R_z measure two cross-components, H_{xy} and H_{xz} , of the magnetic field produced by the T_x transmitter (**1101**). This embodiment of the invention is operable in single frequency or multiple frequency modes.

As an example of the sensitivity to directionality of the 3DEX tool, a bed layer configuration illustrated in **Figure 74** and response value are tabulated in Table 1.

Table 1.

Magnetic field response (A/m)	Case 1	Case 2
Hxx	8.86777008E-04	8.86777008E-04
Hxy	-1.99889226E-04	-1.99889226E-04
Hxz	2.45139177E-04	-2.45139207E-04
Hyy	1.11758942E-03	1.11758942E-03
Hyx	1.99889240E-04	1.99889240E-04
Hyz	-1.41531185E-04	1.41531200E-04
Hzz	1.16889027E-03	1.16889027E-03

The configuration in **Figure 74** is comprised of two cases of three-layered media, labeled Case 1 and Case 2. In both cases, the middle layers **1213** and **1223** are 1 m thick and have a horizontal resistivity (R_h) of 4 Ohm-m and a vertical resistivity (R_v) of 10 Ohm-m. In Case 1, the R_h and R_v are both 1 Ohm-m in the top layer **1211** and 2 Ohm-m in the bottom layer **1215**. In Case 2, the resistivities are interchanged from Case 1, with a R_h and R_v both equal to 2 Ohm-m in the top layer **1221** and 1 Ohm-m in the bottom layer **1225**. In both cases, the relative dip of the borehole is 90 degrees (horizontal borehole) and azimuth angle is 30 degrees. The configuration is shown in **Figure 87**, with T_z pointing out of the page, T_x (**1501**) aligned with its normal at an angle of 30 degrees to the vertical, and T_y (**1502**) aligned with its normal at an angle of 60 degrees to the vertical.

Table 1 shows the magnetic fields responses for the 3DEX instrument taken while positioned in the middle of the center layer. The responses are normalized to a unit transmitter-

receiver moment and are for an excitation frequency of 20 kHz. The normalized field responses are in units A/m. These simple results demonstrate that although H_{xx} , H_{yy} , and H_{zz} are insensitive to directionality, the H_{xy} and H_{xz} components (shown in bold in Table 1) are sensitive to directionality in a horizontal, vertical or deviated wellbore. With this knowledge, a practitioner of the art can discriminate whether a layer is above or below, or on which side of the vertical horizontal or deviated borehole trajectory and thus can use said knowledge for geo-steering purposes.

Figure 88 shows the configuration of the tool used for cases 3 through 11 shown in Figures 75-83. T_z is pointing out of the page as in Figure 87. The transverse transmitters are newly aligned so that the T_x transmitter (1601) is aligned with the normal to the plane of the transmitter along the vertical while the T_y (1602) transmitter is aligned with the normal to the plane of the transmitter along a horizontal direction.

Figure 75 shows a case (Case 3) of a typical anisotropic turbidite layer sequence. The lithology sequence from top to bottom of the model is shale, thick sand, followed by a transition to a low resistivity and electrically anisotropic sand-shale sequence. The resistivities of this bed layer structure are tabulated in Table 2.

Table 2

Resistivity Bed	Depth top boundary (ft)	R _h (ohm-m)	R _v (ohm-m)
1	-10	0.6	0.6
2	0	12	12
3	10	6	6
4	12	3	3
5	14	1.5	5
6	24	0.8	0.8

It is to be noted that **Figures 75-81** do not show tool responses as a tool is moved along a wellbore: in each of the figures, the borehole is horizontal. What is shown is the response of the tool in a horizontal borehole at a specific location in the layered medium given by the horizontal axis in the plots. The sequence contains six overall bed layers, the resistivity of all layers being isotropic except for the fifth bed layer. The anisotropic fifth layer (between 15 and 25 feet of depth) has $R_h = 1.5$ ohm-m and $R_v = 5$ ohm-m. The tool operates at multiple frequencies. Only the 20 kHz response is shown here. In thick beds, when the boundaries are more than 5 feet away from the tool, the H_{xz} response is zero (**1301**). The H_{xz} response starts showing sensitivity to a bed boundary when that bed boundary is within 5 feet of the tool. If the tool is moving from a region of low resistivity to a region of high resistivity, H_{xz} has a negative response (**1303**). Similarly, when the tool is moving from a region of high resistivity to a region of low resistivity, the H_{xz} response is positive (**1305** and **1307**). H_{zz} experiences a positive deflection in the

isotropic (fifth) bed layer (1310), but experiences a larger deflection as the tool enters the isotropic sixth bed layer (1312).

A comparison can be made between Case 3 in **Figure 75** and Case 4 in **Figure 76**.

Figure 76 shows a bed layer structure having a resistivity that is completely isotropic at all bed layers, including an isotropic fifth bed layer. The resistivities of this bed layer structure are tabulated in Table 3.

Table 3

Resistivity Bed	Depth top boundary (ft)	R _h (ohm-m)	R _v (ohm-m)
1	-10	0.6	0.6
2	0	12	12
3	10	6	6
4	12	3	3
5	14	1.5	1.5
6	24	0.8	0.8

In Case 4, R_v and R_h are both equal to 1.5 ohm-m at the fifth bed layer. The H_{xz} component in **Figure 76** is not different substantially from the H_{xz} response in **Figure 3**, even along transitions into and out of the isotropic fifth bed. There is however a noticeable influence on H_{zz} component as the tool crosses the boundary between the fourth and fifth bed layers. Comparing (1310) in **Figure 3** with (1310) in **Figure 3**, shows the dampening effect anisotropy had on the H_{zz} component.

Figure 77 shows a bed layer sequence with a single variation on Case 4 of **Figure 76**. The horizontal and vertical resistivities at the first depth are equal to 2 ohm-m in **Figure 5** whereas the corresponding resistivities are 0.6 ohm-m in **Figure 76**. The resistivities of this bed layer structure are tabulated in Table 4.

5

Table 4

Resistivity Bed	Depth top boundary (ft)	R _h (ohm-m)	R _v (ohm-m)
1	-10	2	2
2	0	12	12
3	10	6	6
4	12	3	3
5	14	1.5	1.5
6	24	0.8	0.8

In the new formation of **Figure 77**, corresponding to the reduced differences in the resistivities of the first and second bed layers, there is less deflection of the H_{xz} component crossing from the first bed to the second bed (503) compared to (403) in **Figure 4**. The magnitude of the negative deflection of H_{zz} (511) is also reduced from it's deflection (411) in **Figure 76**.

The bed layer structure in **Figure 78** shows another single variation on the sequence of **Figure 76**. In **Figure 78**, the sixth depth level has R_h and R_v equal to 2 ohm-m where the resistivity is 0.8 ohm-m in **Figure 76**. The resistivities of this bed layer structure are tabulated in Table 5.

15

Table 5

Resistivity Bed	Depth top boundary (ft)	Rh (ohm-m)	Rv (ohm-m)
1	-10	0.6	0.6
2	0	12	12
3	10	6	6
4	12	3	3
5	14	1.5	1.5
6	24	2	2

Whereas in **Figure 76** the fifth bed layer is more resistive than the sixth bed layer, in **Figure 78** the sixth bed layer is more resistive in all directions than the fifth bed layer. As a result, the deflection of H_{xz} (607) is opposite the direction of the deflection in **Figure 76** (407) across this boundary. As the tool moves from fifth level to the sixth level, the response of the H_{zz} component (610) also reverses its deflected direction from **Figure 76** (410).

Figure 79 shows a linearly graded transition region which lies between 0 and 10 feet between a comparatively low resistivity bed (1 ohm-m) and a comparatively high resistivity bed (11 ohm-m). The resistivities of this bed layer structure are tabulated in Table 6.

Table 6

Resistivity Bed	Depth top boundary (ft)	Rh (ohm-m)	Rv (ohm-m)
1	-10	1	1
2	0	Linear grading	Linear grading
3	10	11	11

At all levels, the resistivity is isotropic. The deflection of H_{xz} depends on the conductivity profile. In the beginning of the transition zone, the deflection of H_{xz} (1703) is large because the slope of the conductivity profile (reciprocal of resistivity) is large. At the end of the zone, the conductivity slope is smaller, and therefore H_{xz} (1705) does not detect the transition into the third bed. Again, the deflection in the entire region is negative because the resistivity is increasing.

Figure 80 shows a case of a thick resistive bed sandwiched between two conductive beds. The sequence corresponds to a top level of shale, a middle thick resistive sand level, and a bottom level of shale. The resistivities of this bed layer structure are tabulated in Table 7.

Table 7

Resistivity Bed	Depth top boundary (ft)	Rh (ohm-m)	Rv (ohm-m)
1	-10	1	1
2	0	10	10
3	10	1	1

The deflection of H_{xz} (801) is negative at the boundary at a depth of 0 feet and has the same order of magnitude as the corresponding deflection in **Figure 75**. Similarly, at the boundary between the beds at 25 feet, the deflection of H_{xz} (803) is positive as the tool crosses into the layer of lower resistivity. H_{zz} responses are also consistent with the results of **Figure 76**.

5 **Figure 81** shows the converse situation from that in **Figure 80**, wherein a conductive bed layer is sandwiched between two resistive bed layers. The resistivities of this bed layer structure are tabulated in Table 8.

Table 8

Conductive Bed	Depth top boundary (ft)	Rh (ohm-m)	Rv (ohm-m)
1	-10	10	10
2	0	1	1
3	10	10	10

10 The H_{xz} signal has a positive deflection (1901) for the boundary at which the resistivity decreases with depth and a negative deflection (1903) where the resistivity increases with depth.

Figures 82 and 83 show graphs of response curves of a horizontal borehole centered at the midpoint (depth of 5 feet) of the second bed layer of **Figure 76**. In the horizontal position, the layer above has different resistivities than the layer below, having consequences for the magnetic responses. The position of the tool is static, and the tool is rotated by 180 degrees about its axis. In **Figure 82**, the tool is operated at 200 kHz. Since the tool is static and horizontal, the H_{zz} (1001) component is constant with rotation. The H_{yy} (1003) and H_{xx} (1005) components oscillate and interchange their values around a mean value as the tool rotates. It can

be shown that the average of H_{xx} and H_{yy} is a constant independent of rotation. However, tool dip, location and the formation type do affect the values of the responses. The angular period of oscillation of H_{xx} and H_{yy} is half a rotation (180°). Likewise H_{xz} (1007) and H_{yz} (1009) also oscillate but have a period of once per full rotation (360°).

5 The graph in Figure 83 results from of the same physical configuration as in Figure 82, except that the tool is operating at 20 kHz. The behavior of all the components is similar to those in Case 10. The angular period of oscillation of H_{yy} (1103) and H_{xx} (1105) is half a rotation (180°). Likewise H_{xz} (1107) and H_{yz} (1109) also oscillate but have a period of once per full rotation (360°). At 20 kHz, the magnitude of the signal response is less than the response at
10 200kHz. Also, in Figure 84, the magnitudes of the H_{xx} (1105) and H_{yy} (1103) components are greater than the magnitude of the H_{zz} (1101) component.

Figure 84 gives a sketch of a 3DEX multi-component induction configuration in a vertical well. The formation comprises a series of horizontal layers alternating between sand (1220) with high total resistivity (high R_t) and shale (1222) with low total resistivity (low R_t).
15 The well bore contains two transmitter coils for illustrative purposes. The upper coil (1201), creates a response (1211) that extends in a plane containing a vertical line. This response would be labeled H_{xx} or H_{yy} and would be a function of R_h and of R_v . The lower (1203) coil creates a response (1213) that lies entirely within a horizontal plane. This response for H_{zz} would be a function of R_h only.

20 Shown in Figure 85a is a resistivity model of a medium with horizontal and vertical resistivities denoted by 1301a and 1301b. The model has three anisotropic intervals indicated as 1303, 1305, and 1307 where the vertical resistivity R_v is greater than the horizontal resistivity R_h . Figure 85b shows the apparent conductivity responses for the H_{xx} (1311) component in the

anisotropic model of Figure 85a. Also shown is the H_{xx} component (1313) for the case of a resistivity model that is isotropic at all depths. The H_{zz} (1315) component of the response for an isotropic model is the same as for the anisotropic model. From Figure 85b, the following observations may be made about the resistivity responses for a vertical well in an anisotropic formation: The H_{zz} response (1315) is not responsive to anisotropy in the formation, while the H_{xx} curves (1311, 1313) are responsive. The H_{xx} response is suppressed by anisotropy. The H_{xx} responses are quite complicated and can even reverse sign close to significant resistivity contrasts. The H_{xx} response may have spikes at bed boundaries.

Figure 86 shows a sketch of a horizontal configuration for a multi-component induction tool. The orientation of the transmitters and receivers remain fixed with respect to the tool. The multi-component tool in horizontal configuration is sensitive to the anisotropic formation, tool location as well as the rotation of the tool around its axis. Only the H_{zz} component is insensitive to tool rotation. In horizontal configuration, the average $0.5 \cdot (H_{xx} + H_{yy})$ is independent of tool rotation. The H_{zz} and $0.5 \cdot (H_{xx} + H_{yy})$ measurements are dependent on the formation and the tool location and thus can be used to determine the distance from the bed boundaries and for geo-steering the invention.

The method of the present invention may be used with data acquired with a logging instrument conveyed on a wireline and also with data acquired using a measurements while drilling (MWD) apparatus conveyed on a drilling tubular such as a drill string or coiled tubing. In particular, when used with MWD measurements, this directional information may be used for controlling the direction of drilling and maintaining the position of the borehole relative to beds in the proximity of the borehole.

A MWD tool conveyed to the borehole will perform measurements with the various transmitter receiver array combinations and configurations. These measurements have azimuthal sensitivity and could be symmetric or asymmetric with respect to the tool axis.

These measurements are deeper electromagnetic data than what is obtained from MWD image tools or other shallow azimuthal tools. In order to improve signal to noise ratio and facilitate interpretation these azimuthal measurements can be organized by depth interval (down to the desired depth resolution) and azimuth sector. **Figure 89** shows a MWD tool 1000 placed in the borehole along the drill path **2206**. This tool travels along the drill path with a vertical velocity $V_z(t)$ and an acceleration $A_z(t)$. The tool also rotates around its longitudinal axis as indicated by arrow **2204** with an angular velocity $w(t)$ and angular acceleration $A_w(t)$. All these dynamic variables can represent the basic tool movements and position inside the borehole. A cross section of the MWD tool shows the azimuthal angular positions within the borehole divided into ten sectors $S(1)$, $S(2)$, through $S(10)$ for example. One azimuthal sector **2202** is shown in this figure. Auxiliary measurements usually made with this type of tool such as inclinometer, gyroscope (fiber, mechanical, etc...), accelerometers (1, 2 and 3 axis), magnetometers provide additional data to recognize the drill path and also the relative position of the tool with respect to the formation while these measurements were performed. With this data available it is possible to bin the measured raw data (RD) in two dimensional bins plus well path and tool position data relative to the formation. The raw data can be organized in depth intervals (n) and azimuth sectors (k) clusters to obtain a raw data array $RD(n,k,t_i)$. The raw data time series assigned to an azimuth sector might not have equal time interval sampling with respect to the transmitter source's periodic repeat cycle since the tool rotation very likely might not be synchronized with this transmitter source periodic repeat cycle. Time averaging of this re-

organized raw data can reduce the signal to noise ratio and improve its accuracy by reducing the standard deviation of the raw data as shown by equations in **Figure 93** for repetitive time domain or frequency domain transmitter sources. The measured raw data time series is clustered in depth intervals, azimuth sector and assigned to a relative time point within the transmitter source's periodic cycle time interval. Optionally in at least one step the tool a portion of the tool could be stationary and pointed in a preferred azimuth direction while the the raw data (RD) time series is acquired. The clustered in bins and averaged data $M(n,k)$ **2208** for each depth interval n and azimuth sector k can form another array in table illustrated in **Figure 90**. During drilling planning the well path is defined along a reservoir geological model with the reservoir physical parameter description including for the resistivity targets associated with the objectives justifying the drilling the well. These resistivity targets have a characteristic response. **Figure 92** shows for example various azimuthal responses for certain multicomponent induction measurements (H_{xx} , H_{yy} , H_{xz} , H_{yz}) to resistivity layers. The averaged data in table shown in **Figure 90** can be used to estimate this expected azimuthal response of the measurement array to a specific formation target of known characteristics and then this estimate can be used to interpret the parameters of the geometry (distance direction thickness) and material properties of this target. All examples shown in **Figure 92** follow a trigonometric sinusoidal function. H_{xx} and H_{yy} have two identical cycles per complete tool rotation and H_{yz} and H_{xz} have one symmetric cycle per tool rotation.

Different targets will have a different function. Failure to properly match the expected functions for a given measurement array and specified formation target could be displayed visually or in a summary report as mismatches are identified (expected versus actual) or error between averaged array data ($M(n,k)$) and function estimate **2210** of the expected relationships associated with expected formation response (**Figure 91**). Actual data for various azimuth sector

and expected functions is illustrated in charts shown in **Figure 92**, which contains four functions (F1 through F4). This information could be used for geo-steering, drilling and well placement decision while drilling.

For time averaging to occur, the transmitter source is preferably periodic with respect to both time domain and frequency domain. As shown in **Figure 94**, the raw data assigned to a depth interval and azimuth sector can fall in different points of the repeat cycle thus, in this case, the time averaging algorithm will average a time series which might not have equal time intervals between sampled points. The tool rotation is not synchronized with a transmitter repeat cycle, however, in an alternative embodiment, the tool rotation can be synchronized with the transmitter repeat cycle. In another embodiment of the method of the present invention, the tool is held stationary while the raw data times are collected. In this case the measuring part of the tool is non-rotating.

The data is interpreted for geo-steering application in association with other acquired microresistivity and image logs such as nuclear, resistivity, and acoustic borehole images. The transmitter can be on the surface or in a nearby well. Flexible circuits are also used in other auxiliary and complementary electromagnetic measurements for both geo-steering and formation evaluation.

The above example of a preferred embodiment has been provided for illustration purposes only and is not intended to limit the scope of the invention, which is determined by the following claims.